

## PCT

## INTERNATIONAL PRELIMINARY EXAMINATION REPORT

(PCT Article 36 and Rule 70)

REC'D 03 DEC 2004



WIPO

PCT

Applicant's or agent's file reference 52016 WO	<b>FOR FURTHER ACTION</b> See Notification of Transmittal of International Preliminary Examination Report (Form PCT/PEA/416)	
International application No. PCT/EP 03/10634	International filing date (day/month/year) 24.09.2003	Priority date (day/month/year) 25.09.2002
International Patent Classification (IPC) or both national classification and IPC G01L3/10		
Applicant FAST TECHNOLOGY AG. et al.		

1. This international preliminary examination report has been prepared by this International Preliminary Examining Authority and is transmitted to the applicant according to Article 36.
2. This REPORT consists of a total of 4 sheets, including this cover sheet.  
  
☐ This report is also accompanied by ANNEXES, i.e. sheets of the description, claims and/or drawings which have been amended and are the basis for this report and/or sheets containing rectifications made before this Authority (see Rule 70.16 and Section 607 of the Administrative Instructions under the PCT).  
  
 These annexes consist of a total of sheets.

3. This report contains indications relating to the following items:
  - I ☒ Basis of the opinion
  - II ☐ Priority
  - III ☒ Non-establishment of opinion with regard to novelty, inventive step and industrial applicability
  - IV ☐ Lack of unity of invention
  - V ☐ Reasoned statement under Rule 66.2(a)(ii) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement
  - VI ☐ Certain documents cited
  - VII ☐ Certain defects in the international application
  - VIII ☐ Certain observations on the international application

Date of submission of the demand  29.03.2004	Date of completion of this report  02.12.2004
Name and mailing address of the international preliminary examining authority:   European Patent Office D-80298 Munich Tel. +49 89 2399 - 0 Tx: 523656 epmu d Fax: +49 89 2399 - 4465	Authorized Officer  Coda, R  Telephone No. +49 89 2399-2802  

**INTERNATIONAL PRELIMINARY  
EXAMINATION REPORT**

International application No. **PCT/EP 03/10634**

**I. Basis of the report**

1. With regard to the **elements** of the international application (*Replacement sheets which have been furnished to the receiving Office in response to an invitation under Article 14 are referred to in this report as "originally filed" and are not annexed to this report since they do not contain amendments (Rules 70.16 and 70.17)*):

**Description, Pages**

1-16 as originally filed

**Claims, Numbers**

1-14 as originally filed

**Drawings, Sheets**

1/7-7/7 as originally filed

2. With regard to the **language**, all the elements marked above were available or furnished to this Authority in the language in which the international application was filed, unless otherwise indicated under this item.

These elements were available or furnished to this Authority in the following language: , which is:

- ☐ the language of a translation furnished for the purposes of the international search (under Rule 23.1(b)).
- ☐ the language of publication of the international application (under Rule 48.3(b)).
- ☐ the language of a translation furnished for the purposes of international preliminary examination (under Rule 55.2 and/or 55.3).

3. With regard to any **nucleotide and/or amino acid sequence** disclosed in the international application, the international preliminary examination was carried out on the basis of the sequence listing:

- ☐ contained in the international application in written form.
- ☐ filed together with the international application in computer readable form.
- ☐ furnished subsequently to this Authority in written form.
- ☐ furnished subsequently to this Authority in computer readable form.
- ☐ The statement that the subsequently furnished written sequence listing does not go beyond the disclosure in the international application as filed has been furnished.
- ☐ The statement that the information recorded in computer readable form is identical to the written sequence listing has been furnished.

4. The amendments have resulted in the cancellation of:

- ☐ the description, pages:
- ☐ the claims, Nos.:
- ☐ the drawings, sheets:

**INTERNATIONAL PRELIMINARY  
EXAMINATION REPORT**

International application No. **PCT/EP 03/10634**

5. ☐ This report has been established as if (some of) the amendments had not been made, since they have been considered to go beyond the disclosure as filed (Rule 70.2(c)).

*(Any replacement sheet containing such amendments must be referred to under item 1 and annexed to this report.)*

6. Additional observations, if necessary:

**III. Non-establishment of opinion with regard to novelty, inventive step and industrial applicability**

1. The questions whether the claimed invention appears to be novel, to involve an inventive step (to be non-obvious), or to be industrially applicable have not been examined in respect of:

☐ the entire international application,

☒ claims Nos. 1-14

because:

☐ the said international application, or the said claims Nos. relate to the following subject matter which does not require an international preliminary examination (specify):

☒ the description, claims or drawings (*indicate particular elements below*) or said claims Nos. 1-14 are so unclear that no meaningful opinion could be formed (*specify*):

**see separate sheet**

☐ the claims, or said claims Nos. are so inadequately supported by the description that no meaningful opinion could be formed.

☐ no international search report has been established for the said claims Nos.

2. A meaningful international preliminary examination cannot be carried out due to the failure of the nucleotide and/or amino acid sequence listing to comply with the standard provided for in Annex C of the Administrative Instructions:

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**Re Item III**

**Non-establishment of opinion with regard to novelty, inventive step and industrial applicability**

1. Although claims 1, 7, 11 and 13 have been drafted as separate independent claims, they appear to relate effectively to the same subject-matter and to differ from each other only with regard to the definition of the subject-matter for which protection is sought and in respect of the terminology used for the features of that subject-matter. The aforementioned claims therefore lack conciseness. Moreover, lack of clarity of the claims as a whole arises, since the plurality of independent claims makes it difficult, if not impossible, to determine the matter for which protection is sought, and places an undue burden on others seeking to establish the extent of the protection. Hence, claims 1, 7, 11 and 13 do not meet the requirements of Article 6 PCT.
2. In order to overcome this objection, it would appear appropriate to file an amended set of claims defining the relevant subject-matter in terms of a single independent apparatus claim followed by dependent claims covering features which are merely optional (Rule 6.4 PCT).
3. In view of the above objection it is not at present practicable to carry out a full examination of the application. A preliminary examination of the independent claim 1, which is considered to be the broadest independent claim of the application, has been however carried out.  
The subject-matter of claim 1 is not new (Art. 33(2) PCT). In fact, document D1 (US4882936) discloses a torque transducer (see column 1, lines 11 to 14) having: a shaft subject to torque about a longitudinal axis, a transducer element integral with the shaft and remanently magnetised to emanate a component of magnetic field dependent on the torque applied to the shaft (see column 8, lines 1 to 8; figure 1(2, 6, 8)), a sensor coil disposed about the shaft to generate a signal dependent of the applied torque (see column 13, lines 39 to 48, 52 to 59; column 4, lines 1 to 9; figure 1(20, 24)), a load connected to the coil to enable a current to circulate in the coil (see column 14, lines 18 to 40) and a receiver responsive to the field emanated by the coil to generate a torque dependent signal (see column 13, lines 56 to 59).  
In particular, it is noted that at column 26, lines 3 to 14 it is disclosed the possibility of having a receiver which is remote from the coil.

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(PCT Article 36 and Rule 70)



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Name and mailing address of the international preliminary examining authority:   European Patent Office D-80298 Munich Tel. +49 89 2399 - 0 Tx: 523656 epmu d Fax: +49 89 2399 - 4465	Authorized Officer  Coda, R  Telephone No. +49 89 2399-2802  

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International application No. **PCT/EP 03/10634**

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**INTERNATIONAL PRELIMINARY  
EXAMINATION REPORT**

International application No. **PCT/EP 03/10634**

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because:

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In particular, it is noted that at column 26, lines 3 to 14 it is disclosed the possibility of having a receiver which is remote from the coil.



## PATENT COOPERATION TREATY

PCT

NOTIFICATION CONCERNING  
SUBMISSION OR TRANSMITTAL  
OF PRIORITY DOCUMENT

(PCT Administrative Instructions, Section 411)

From the INTERNATIONAL BUREAU

To:

THOMAS, Kurig  
Becker, Kurig, Straus  
Bavariastrasse 7  
80336 München  
GermanyBECKER (KURIG STRAUS)  
BAVARIASTRASSE 7 80336 MÜNCHEN

13. Jan. 2004

WV: ..... / LF: .....

Date of mailing (day/month/year) 29 December 2003 (29.12.03)	<b>IMPORTANT NOTIFICATION</b>
Applicant's or agent's file reference 52016 WO	
International application No. PCT/EP03/10634	
International publication date (day/month/year) Not yet published	
Applicant FAST TECHNOLOGY AG. et al	International filing date (day/month/year) 24 September 2003 (24.09.03)  Priority date (day/month/year) 25 September 2002 (25.09.02)

- The applicant is hereby notified of the date of receipt (except where the letters "NR" appear in the right-hand column) by the International Bureau of the priority document(s) relating to the earlier application(s) indicated below. Unless otherwise indicated by an asterisk appearing next to a date of receipt, or by the letters "NR", in the right-hand column, the priority document concerned was submitted or transmitted to the International Bureau in compliance with Rule 17.1(a) or (b).
- This updates and replaces any previously issued notification concerning submission or transmittal of priority documents.
- An asterisk (\*) appearing next to a date of receipt, in the right-hand column, denotes a priority document submitted or transmitted to the International Bureau but not in compliance with Rule 17.1(a) or (b). In such a case, the attention of the applicant is directed to Rule 17.1(c) which provides that no designated Office may disregard the priority claim concerned before giving the applicant an opportunity, upon entry into the national phase, to furnish the priority document within a time limit which is reasonable under the circumstances.
- The letters "NR" appearing in the right-hand column denote a priority document which was not received by the International Bureau or which the applicant did not request the receiving Office to prepare and transmit to the International Bureau, as provided by Rule 17.1(a) or (b), respectively. In such a case, the attention of the applicant is directed to Rule 17.1(c) which provides that no designated Office may disregard the priority claim concerned before giving the applicant an opportunity, upon entry into the national phase, to furnish the priority document within a time limit which is reasonable under the circumstances.

<u>Priority date</u>	<u>Priority application No.</u>	<u>Country or regional Office or PCT receiving Office</u>	<u>Date of receipt of priority document</u>
25 Sept 2002 (25.09.02)	0222296.6	GB	12 Dec 2003 (12.12.03)

The International Bureau of WIPO  
34, chemin des Colombettes  
1211 Geneva 20, Switzerland

Facsimile No. (41-22) 338.89.70

Authorized officer

Maria KIRCHNER (Fax 338 8970)

Telephone No. (41-22) 338 8056

# PATENT COOPERATION TREATY

From the  
INTERNATIONAL PRELIMINARY EXAMINING AUTHORITY

## PCT

To:

STRAUS, Alexander  
BECKER, KURIG, STRAUS  
Bavariastrasse 7  
D-80336 München  
ALLEMAGNE

BECKER KURIG STRAUS  
BAVARIASTRASSE 7 · 80336 MÜNCHEN

06. Dez. 2004

WV: ..... / LF: .....

NOTIFICATION OF TRANSMITTAL OF  
THE INTERNATIONAL PRELIMINARY  
EXAMINATION REPORT

(PCT Rule 71.1)

Date of mailing  
(day/month/year)

02.12.2004

Applicant's or agent's file reference  
52016 WO

### IMPORTANT NOTIFICATION

International application No.  
PCT/EP 03/10634

International filing date (day/month/year)  
24.09.2003

Priority date (day/month/year)  
25.09.2002

Applicant  
FAST TECHNOLOGY AG. et al.

1. The applicant is hereby notified that this International Preliminary Examining Authority transmits herewith the international preliminary examination report and its annexes, if any, established on the international application.
2. A copy of the report and its annexes, if any, is being transmitted to the International Bureau for communication to all the elected Offices.
3. Where required by any of the elected Offices, the International Bureau will prepare an English translation of the report (but not of any annexes) and will transmit such translation to those Offices.
4. **REMINDER**

The applicant must enter the national phase before each elected Office by performing certain acts (filing translations and paying national fees) within 30 months from the priority date (or later in some Offices) (Article 39(1)) (see also the reminder sent by the International Bureau with Form PCT/IB/301).

Where a translation of the international application must be furnished to an elected Office, that translation must contain a translation of any annexes to the international preliminary examination report. It is the applicant's responsibility to prepare and furnish such translation directly to each elected Office concerned.

For further details on the applicable time limits and requirements of the elected Offices, see Volume II of the PCT Applicant's Guide.

The applicant's attention is drawn to Article 33(5), which provides that the criteria of novelty, inventive step and industrial applicability described in Article 33(2) to (4) merely serve the purposes of international preliminary examination and that "any Contracting State may apply additional or different criteria for the purposes of deciding whether, in that State, the claimed inventions is patentable or not" (see also Article 27(5)). Such additional criteria may relate, for example, to exemptions from patentability, requirements for enabling disclosure, clarity and support for the claims.

Name and mailing address of the international  
preliminary examining authority:



European Patent Office  
D-80298 Munich  
Tel. +49 89 2399 - 0 Tx: 523656 epmu d  
Fax: +49 89 2399 - 4465

Authorized Officer

Püschel, S


Tel. +49 89 2399-5812



# PATENT COOPERATION TREATY

## PCT

### INTERNATIONAL PRELIMINARY EXAMINATION REPORT (PCT Article 36 and Rule 70)

Applicant's or agent's file reference 52016 WO		<b>FOR FURTHER ACTION</b> See Notification of Transmittal of International Preliminary Examination Report (Form PCT/IPEA/416)	
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International application No. PCT/EP 03/10634

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**INTERNATIONAL PRELIMINARY  
EXAMINATION REPORT - SEPARATE SHEET**

International application No. PCT/EP 03/10634

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In particular, it is noted that at column 26, lines 3 to 14 it is disclosed the possibility of having a receiver which is remote from the coil.

Title: Torque Signal Transmission

FIELD OF THE INVENTION

5 This invention is concerned with a method of and apparatus for the sensing of torque and the transmission of a torque-dependent signal to a remote measurement apparatus by a wireless technique. In this content, wireless transmission means signal transmission without the need of a cable or other like physical connection.

10 The invention finds particular utility in a torque-generating system in which the torque is generated as pulses of torque. An example of such pulse torque generation is in power fastening tools for fastening or tightening nuts onto bolts or studs for example. Power fastening tools find application in many industries, a major one of which is automobile assembly.

BACKGROUND TO THE INVENTION

15 The measurement of torque applied to a fastening, such as a nut and bolt, has long presented problems in determining the point at which a desired torque value is achieved when using pulse-type power torque tools. Among the techniques developed for measuring pulsed torque are those based on magnetic transducer technology in which a magnetised transducer is  
20 incorporated in or coupled to a torque transmission shaft in a power tool and a torque-dependent magnetic field component is sensed by a non-contact sensor arrangement to develop a torque-representing signal which is transmitted by an electrical connection to signal-processing circuit. The complete torque measuring assembly can be mounted in the tool. An  
25 alternative is to transmit a torque-dependent signal from the tool to a remote signal processing circuit as by a cable or wire connection. Even if the signal

were to be transmitted by a wireless connection, e.g. an infra-red link, it is necessary to provide power to the tool end of the link.

There would be considerable benefit in a torque sensor with remote signalling to a processor which did not require electrical power to be provided in association with the sensor. A torque sensor of this kind would be of particular value applied in a power torque tool adaptor of the kind described in British patent application GB 0219745.7 filed 23<sup>rd</sup> August 2002 which is incorporated herein by reference and to which further reference will be made below.

- 10 The application of magnetic transducer technology for torque measurement in a power impact tool is disclosed in U.S. patent 6 311 786 and in its published continuation application US 2002/0020538 in which torque measurement and control is contained within the tool. The torque transducer uses a ferromagnetic sensor and specifically discloses a magneto-elastic ring coupled to the output shaft of the tool. An impact tool control method and apparatus is described in International patent application publication WO01/44776. The control system uses a magneto-elastic torque transducer mounted exteriorly of the tool in which the magneto-elastic transducer element is an integral portion of a shaft through which torque is transmitted.
- 15 20 This document also discloses the implementation of the control system as a retrofit system for use in controlling an existing impact tool. The magnetic field generated by the transducer element is detected by a detector which can be a coil of wire circumferentially arranged around the transducer or other device. The coil is connected into the input of an integrator in a signal processing circuit.
- 25

The PCT patent application PCT/EP02/06960 filed 24<sup>th</sup> June 2002, the disclosure of which is incorporated herein by reference, discloses the control of a pulsed torque tool using a magnetic-based torque transducer which has a



transducer element or region integral with the output shaft of the tool. The control apparatus including the transducer is disposed interiorly of the power torque tool.

5 Above-mentioned application GB 0219745.7 describes an adaptor attachable to a conventional power torque tool of the pulsed-type whereby torque measurement and control can be exercised on the tool. In GB 0219745.7 the adaptor is connected to a unit containing external circuitry by a cable. It may be coupled by a wire-less link, e.g. an IR link, to transmit a torque-dependent signal to the external unit but in that case, the adaptor requires electrical  
10 power for its operation.

#### SUMMARY OF THE INVENTION

One aspect of the present invention is based on the concept of transmitting a torque-dependent signal to a remote unit by means of an emanated field. In particular it is applied to modify an adaptor of the kind described in GB  
15 0219745.7 so that the adaptor is active in the sense of being magnetically active to generate the torque-dependent signal but is passive in the sense of not requiring a source of electrical power.

Another aspect of the invention is based on the concept of deriving an electrical power supply from torque pulses to power a signalling system for  
20 transmission to a remote unit and, if appropriate, to power a sensor arrangement.

Aspects and features of the present invention are set forth in the claims following this description.

The invention and its practice will be further described with reference to an  
25 embodiment illustrated in the accompanying drawings.

### BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 illustrates an adaptor for fitting to a power torque tool to transmit a torque-dependent signal in accord with the present invention;

5 Fig. 2 illustrates the internal construction of an adaptor based on that disclosed in GB 0219745.7

Fig. 3 shows a shaft with an integral magnetised transducer region and a sensor coil;

Fig. 4 is a response curve as a function of the axial position of the sensor coil for a transducer region having profile-shift longitudinal magnetisation;

10 Fig. 5 shows the connection of the arrangement of Fig. 3 with a power supply and signal transmission circuit, all energised by sensed torque pulses;

Fig. 6 shows a modification of the arrangement of Fig. 3 to use a capacitive load;

15 Fig. 6a shows the circuit used to investigate the "resonance" effect of a capacitive load;

Figs. 7a to 7c are response curves to pulse torques of lower, medium and higher torque respectively using the circuit of Fig. 6a;

Fig. 8 shows a simplified illustration of a torque adaptor to which a coil sensor is applied;

20 Fig. 9 is a preferred coil arrangement for use with the response curve of Fig. 4 and

Fig. 9a is the preferred connection of the two coil sections of the coil arrangement of Fig. 9.

### DESCRIPTION OF THE PREFERRED EMBODIMENTS

Fig. 1 shows a conventional power torque tool 10, such as an impact-type fastening tool which provides torque pulses at an output shaft 12. The tool may also be of the type in which pulses are generated by controlled actuation of a piston and cylinder mechanism. The tool illustrated is powered by compressed air through line 14. It is conventional to fit a load-engaging adaptor on the end 12a of the shaft 12 distal the power tool for transmitting torque to the load, e.g. a nut or bolt head. Such an adaptor is exemplified in PCT/EP02/06960. The adaptor is a passive mechanical article for transmitting torque from the shaft to the load. As above-mentioned in the system described in PCT/EP02/06960, torque measurement and control is performed within the tool body 10.

In the illustrated embodiment of the present invention a torque sensor adaptor 20 is provided to enable torque measurement and control to be exercised on a conventional pulsed torque tool not containing such provision. The adaptor 20 couples to the tool output shaft at one end and receives a conventional passive adaptor for engaging a load at the other end. The adaptor incorporates a torque transducer arrangement using a magnetic-based torque transducer element. The adaptor 20 can be characterised as an active device in contrast to prior passive devices. However, as will become clear hereinafter, the adaptor is magnetically active as regards torque sensing but is passive in the sense of requiring no electrical power supply for operation. The adaptor 20 emanates a field carrying a torque-dependent signal as indicated by arrow 50 which is received by a remote receiver unit 52. Unit 52 is connected by cable connection 22 to a signal processing and controller unit 30 which in turn supplies a shut-off signal over cable connection 32 to an air-valve unit 40 acting in line 14. The unit 30 may include a display 34, e.g. an LCD display, for displaying relevant parameters on a manually actuable key pad 36 for entering control instructions and data to a programmed

microprocessor (not shown) housed in unit 30. The unit 30 can be mounted or carried so as to be free of the vibration generated in operation of the tool 10. The receiver unit 52 may be included within unit 30. As schematically illustrated by chain lines 24 the adaptor 20 has a body portion 26 which is securable or attachable to the body of the power tool 10 as will be described below. The adaptor has a torque transmitting shaft extending through the body and having an output end 28.

Fig. 2 shows one form of construction for the adaptor 20 which is constructed to transmit torque about an axis A-A. It is a general aim of the construction to keep the axial length of the torque transmitting shaft as short as possible. The adaptor has a housing 26 with an internal circular bore 27 in which is mounted a torque transmitting transducer assembly 60 rotatable within the housing 26 about central axis A-A.

The assembly 60 has a shaft portion 62 disposed between an input portion 64 and an output portion 66 providing the output end 28 of Fig. 1. The input and output roles are reversible but the shaft portions 62 and 64 are shaped in accord with usual power tool practice. The input portion 64 is configured for engagement with the shaft 12 of tool 10. It is of larger diameter than the shaft portion 62 and includes an axial blind bore 68 configured to fit on the distal end 12a of the tool output shaft 12. For example, if the tool output shaft is of a square cross-section, the bore 68 is of a matching square section. The output portion 66 is shown in this embodiment as a square cross-section shaft similar to the output shaft 12 of the power tool and to which a passive load-engaging adaptor can be fitted. It will be understood that the input and output portions of the assembly 60 can be configured as required by the tool and the load adaptor respectively; or the output portion 66 could be configured for direct engagement with the load.

The shaft portion 62 is of circular cross-section and is radially-spaced from the adjacent inner surface of housing 26. Shaft portion 62 is magnetised at 70 to provide a torque-sensitive transducer element or region which emanates a torque-dependent magnetic field which is sensed by a sensor arrangement to be described and not shown in Fig. 2.

The region 70 is a region of stored magnetisation. That is, it is remanently magnetised to store a permanent magnetisation. Preferably the magnetisation is an annulus of longitudinal magnetisation about axis A-A. the longitudinal magnetisation is in the direction of axis A-A, e.g. as illustrated N-S. The longitudinal magnetisation may be of the kind known as circumferential sensing as disclosed in WO01/13081 or, preferably, of the kind known as profile-shift (axial or radial sensing) as disclosed in WO01/79801. Another torque measuring technique which does not require a region of stored magnetisation is that disclosed in British patent application GB 0204213.3 filed 22<sup>nd</sup> February, 2002. In this technique the transducer element is not a previously magnetised or (encoded) region of the shaft but is a defined region in which the torque-sensitive element is established in use.

Looking at further details of the constructions of the adaptor of Fig. 2, the output portion of square cross section includes recess 65 for co-operating with a standard passive mechanical adaptor. The transducer region 62 is located for rotation within the housing by a plain bearing provided by an annular bush 80 of a plastics material which is bonded to or otherwise secured against rotation to a forward (i.e. toward the output end) inside surface 27a of the housing 26. The interior diameter of bush 80 is slightly greater than the diameter of region 62, other than for a forward lip 82 which bears against the shaft.

The rearward end of bush 80 seats against an internal step 27b of housing 26 and also provides an abutment 84 for axially locating the transducer assembly

and specifically a forward surface of the enlarged input portion 64. The input portion is sized to rotate freely within a part 26a of the housing of reduced internal diameter extending from step 27b to a rearward internal step 27c. Step 27c lies adjacent a circumferential groove 67 in the input portion 64. An  
5 annular bushing 86 of a low friction, self-lubricating material is received in the groove and engages the interior surface of housing 26 and is axially located by step 27c. The bushing 86, and therewith the transducer assembly 60 is retained in the housing by an internally-located press-fit retaining ring 88 at the rear of the housing. The housing 26 not only provides mechanical  
10 support and protection but provides a magnetic shield for the transducer assembly. It will be understood that the construction illustrated in Fig. 2 is diagrammatic in nature.

One feature of the assembly 60 of Fig. 2 is that the input portion 64 terminates at 64a flush with the rearward end 26b of the housing 26 or within the axial  
15 confines of the housing which is in accord with the desire to keep the overall length of the active adaptor as small as possible. The square-section bore 68 for engaging the output shaft of the power tool is contained within the housing. The assembly 60 is a push fit into the housing 26 from its rearward end.

20 To perform the function generally indicated at 24 in Fig. 1 of preventing rotation of the adaptor housing and to retain the output shaft 12a of the power tool engaged within the bore 68, the exterior of housing 26 is adapted to retain one end of a stiff helical spring (or more than one such spring) the other end of which is retained on the housing of the power tool. The spring, thus  
25 retained, is in an axially stretched state (in tension) so that the tension maintains the active adaptor engaged with the power tool. It has also been found that the flexibility of the retaining spring enables the power tool fitted with the active adaptor to accommodate the variations in the angle between the torque axis and the load being fastened that occur in practical use of the

tool. It will be understood the plain bearing type of rotary support provided by bush 80 and bushing 86 could be substituted by other means of bearing support.

The description given so far with reference to Figs. 1 and 2 closely follows the description of the adaptor disclosed in GB 0219745.7. Attention will now be given to the modifications to that design by which the present invention is implemented.

Referring to Fig. 1, in GB 0219745.7 the adaptor 20 is connected directly to the processing unit by cable 22. The adaptor houses a magnetic field sensor arrangement co-acting with a transducer region which is connected via cable 22 into a signal conditioning circuit in unit 30; or which is connected to a signal conditioning circuit within the adaptor which circuit then transmits a torque-representing signal to the unit 30 over cable 22. Either way, the operation of the sensor devices in adaptor 20 requires electrical power to be supplied in or to the adaptor. The substitution of a wire-less link, e.g. an infra-red (IR) link, for the cable 22 would still require the supply of power in or to the adaptor. The foregoing disadvantage can be obviated by the torque sensing and signal sending techniques now to be described. The technique is of general utility and is not restricted to being applied to the adaptor under specific consideration.

Fig. 3 shows a ferromagnetic shaft 100 rotatable about a longitudinal axis A-A. An integral portion 70 of the shaft is encoded with a remanent, annular magnetisation of the kind referred to a profile-shift as described in above-mentioned WO01/96826. A single coil is wound closely about the shaft. For the purposes of the immediate discussion the coil is movable axially with respect to the region 70. The coil is terminated in a low value resistor R, of say 270 $\Omega$ . Fig. 4 shows a graph of the voltage across the resistor (current induced to circulate in the coil) as a function of the axial position of the coil

relative to region 70 when the transducer region is subject to a torque pulse of a given value. Current is induced in the coil by the resultant torque-dependent change in the magnetic flux distribution acting on the coil. M The coil current is proportional to the rate of change of flux during the torque impulse. By way of example, the encoded region 70 may be 22 mm wide and the width of the coil 4-5 mm with the coil having 300 turns or more.

When a torque pulse is applied to one end shaft 100, it propagates along the shaft "winding up" the shaft. There is then a lesser recoil pulse of opposite polarity dependent on the elasticity of the shaft material. This phenomenon will appear in torque pulse graphs described later.

Reverting to Fig. 4 it will be seen that the voltage across resistor R is at a maximum at two points 72a, 72b spaced from the centre-line 74 of the region 70. The polarity reverses as the coil passes through alignment with the centre line and investigation thus far has revealed that the maximum voltages are achieved when the coil is aligned with the sweet spots described in WO01/96826 with reference to Fig. 30 thereof.

The voltage/current induced in the coil 110 has two possible functions. The first is as a source of electrical energy. That is the transducer provides a mechanical(torque)-to-electrical energy converter. The second is as a torque-dependent signal usable in a subsequent torque measurement and control process. Fig. 5 is a diagrammatic illustration of the use of the voltage/current induced in the coil for both possibilities.

In Fig. 5 the coil 110 is connected to a power control unit 112 which generates a supply voltage  $V_s$  at terminal 114. The unit 112 may include a rectifier arrangement, connected across the coil to develop a usable power supply voltage from the voltage at the coil terminals. The rectifier arrangement is preferably of the full wave bridge type to use excursions of both polarities of the coil output voltage. The rectifier arrangement feeds a smoothing



capacitor to derive a smoothed unipolar voltage from the rectifier arrangement and a low power voltage regulator device may also be employed. The supply voltage  $V_s$  is used to power the torque signal transmission part of the arrangement of Fig. 5.

- 5 The torque-dependent signal voltage developed across the coil is applied as the input to a signal conditioning circuit 120 which processes the signal to generate a torque signal  $V_T$  which modulates a transmitter unit 122 to transmit the torque-representing signal by any form of wireless connection 50, such as light (visible or otherwise), radio, sound, induction etc.
- 10 The coil 110 may be tightly wrapped around the region 70 of shaft 100 at an axial position at which maximum energy output is generated, e.g. a sweet spot as discussed with reference to Fig. 4. Consequently if the coil is to rotate with the shaft and if the shaft is to continue to rotate under successive torque pulses, it may be necessary to connect the coil to the remainder of the
- 15 circuitry through slip rings. Alternatively the coil 110 may be wound sufficiently spaced from the shaft to allow the shaft to rotate within a fixed coil. The shaft may be a steel of the type mentioned below.

A presently preferred embodiment of the invention will now be described which makes use of remote signalling but does not require the provision of a

20 power supply to energise a transmitter device. This implements the second function mentioned above.

It will be noted that the power generating function of the coil 110 could be used for powering a magnetic field sensor arrangement using sensor devices such as saturating core inductors, Hall effect devices or

25 magnetoresistive devices. The torque-dependent signal thereby obtained modulates transmitter unit 122 for remote signalling as already described.

Fig. 6 is similar to Fig. 3 but shows a capacitor C connected across the coil 110. The coil may be in the range of 300 to 600 turns on a 15-18 mm diameter shaft of FV 250B steel. Other suitable steels are those known under the designations S155, S156 and 14 NiCo14. The steels have to be chosen for a combination of the mechanical properties required for the torque transmission system in which they are employed and their magnetic properties for sustaining the transducer region 70 and providing a torque-dependent magnetic field component.

It has been found that such a circuit can produce a resonance which causes the coil 110 to emanate a field 50, which is detectable at some distance away. The resonance may serve to amplify the current generated in the coil. The resonance may be at a harmonic frequency related to the pulse period. The radiated field can be detected with the aid of a receiving coil 130 of say 600 turns wound on a ferrite rod. The signal has, for example, been detected on a long-wave radio using a ferrite rod aerial, that is a radio tuned in the range 150-300 kHz. The emanated field from coil 110 has been detected over a range of 30 cms up to 1.5 m.

This resonance effect has been investigated with the coil circuit shown in Fig. 6a in which the coil 110 is connected to a resonating capacitor C of  $1\mu\text{F}$  in series with a resistor R of  $270\ \Omega$ . The voltage across the coil is displayed in conjunction with a separate measurement of the torque acting on the transducer region. Figs. 7a, 7b and 7c are graphical displays of the detected signals for lower, medium and higher torque values respectively. The measured torque signal is the upper trace in each case, the voltage  $V_c$  across the coil is the lower trace. The coil voltage polarity is inverted which is an artifact of the instrumentation used.

The torque pulse T shows as a positive going portion  $T^+$  followed by a negative going portion  $T^-$  which represents the recoil due to mechanical

- energy stored in the shaft by the applied torque. The magnitude of the recoil pulse  $T$  depends on the amount of rotation of the shaft in response to the applied torque and associated energy losses. The "torque pulse" acting on coil 110 is in the form of the torque-dependent magnetic flux generated by the transducer region 70. The coil voltage/current is primarily responsive to the rate of change of flux as already noted, that is the rate of change of the torque pulse  $T$ . It should be said that the precise nature of the torque pulse as applied to fastening a nut and bolt when the two are becoming tight is a complex subject.
- 10 The coil voltage  $V_c$  is in the nature of a double pulse, having two pulses  $V_1$  and  $V_2$  of opposite polarity which relate to the slope of the rising part of the applied torque pulse  $T$  and the slope of the relaxation part of the torque pulse respectively. It has been found that for torque pulses, the peak height of the coil signal is proportional to the amount of torque applied during the torque pulse. The steepness of the torque pulse slope is dependent on the initial pulse as generated, e.g. by a power torque tool, the load acting on the shaft and the shaft material, that is the elasticity of the shaft. The voltage  $V_c$  across the coil has been found to be in a range of a few to several hundred millivolts which is significant.
- 20 The teachings given above for both functions mentioned have related to investigations with the profile-shift form of longitudinal magnetisation described in WO01/96826. However, other magnetisations which produce torque-dependent magnetic fields may be treated in a similar way. Reference has already been made to circumferential-sensing longitudinal magnetisation described in WO01/13081 and circumferential or circular magnetisation in a magneto-elastic material such as disclosed in U.S. patents 5 351 555 and 5 465 627 and SAE Technical Paper Series 920707 published by the Society of Automotive Engineers under the title "Development of a Non-Contact Torque Transducer for Electric Power Steering Systems".

Circumferential magnetisation can also be used in an integral portion of a shaft. As will be described below the response obtained with longitudinal magnetisation of the kind described in WO01/96826 and on which the response of Fig. 4 is founded, can be utilised in a particularly beneficial way by using a two-coil sensor.

However, continuing with the single coil sensor so far discussed, its application to the adaptor of Figs. 1 and 2 will now be described. Fig. 8 shows a torque-detecting adaptor for a power torque tool such as illustrated in Fig. 2. The earlier description of Fig. 2 did not describe the sensor arrangement which coacts with transducer region 70. A coil sensor arrangement based on the teachings of Figs. 3 and 4 is shown in Fig. 8 in which the adaptor is shown in simplified form. The housing 26, which may be of enlarged radial thickness, is provided with an external groove in which the coil 110 is seated and retained to sense the field emanated by the region 70 of shaft portion 62 (Fig. 2). The coil 110 is not in contact with the shaft in the adaptor which is free to rotate within the coil. The coil should be positioned axially at a sweet spot 72a or 72b of Fig. 4. For the coil 110 to coact with region 70, the material of housing 26 (and bush 82) should not be of a magnetic material so that the coil is properly influenced by the field emanated by region 70.

An alternative is illustrated in Fig. 2 itself in which the coil indicated as 110' is embedded within the bush 82. The coil can be positioned radially close to transducer region 70 but without actually contacting the region. In order to emanate a field from the coil to communicate with the receiver unit 52 of Fig. 1, the housing 26 should be of a material that does not adversely screen the emanated field. The receiver unit 52 employs a coil wound on a ferrite rod as described with reference to Fig. 6.

To make better use of the response characteristic of Fig. 4, the modification shown in Fig. 9 is preferred. The single coil 110 is substituted by two spaced coils 110a and 110b, each aligned with a respective sweet spot 72a, 72b. The coils are connected as shown in Fig. 9a so that the resultant voltage  $V_c$  is the sum of the magnitudes of the respective coil voltages. By way of example, for a region 70 that is 22 mm wide, the sweet spots were found to be 14 to 15 mm apart. The axial centres of coils 110a, 110b were equally spaced apart, each coil being 4-5 mm long. The signal output voltage can be expected to be in the range of 0.5-1V when using 2 x 300 turn coils on a shaft of 15-18 mm diameter of FV 250B steel, the coils being terminated in a resistor R.

In accordance with the earlier discussion it is preferred to place a "resonating" capacitor, or a series CR combination, across the series connected coils as indicated in Fig. 9a. The additional component(s) are part of the adaptor and, for example, could be embedded in bush 82 as well as coils 110a and 110b.

The resultant adaptor is of rugged construction to meet the high vibration environment in which it is used and requires the minimum of components.

One problem arising out of remote signalling is that the magnitude of a received signal will be a function of distance between the transmitter and the receiver unit. The received signal level will be expected to vary as the inverse square of the distance. Thus unless the signal receiver is maintained at a fixed distance at which a calibration can be made, the magnitude of the received signal is not correlated with the torque that is being measured.

A solution to this problem is to provide the transmitted signal with its own internal reference. Fig. 10 illustrates one solution. It shows a dual polarity pulse output such as is seen in Figures 7a-7c (lower trace) representing the coil voltage  $V_c$ . One of the pulse pair is clipped to a fixed amplitude, as by a Schottky diode clipper. This is shown on the second pulse of the pair where

the clipping level is indicated at  $V_L$ . This provides a reference against which the amplitude of the first pulse of the pair is measurable.

5 A second solution is to use a signal, other than the torque pulse, that is generated by the torque pulse source. For example, in impact power torque tools it has been noticed that the hammer mechanism generates a signature torque signal which is separate from the desired torque impulses. This is illustrated in Fig. 11 in which the signature signal  $S$  of a constant amplitude lies between the torque pulses of varying amplitude. This provides the reference.

Claims

1. A torque transducer comprising:
  - a shaft subject to torque about a longitudinal axis;
  - a transducer element integral with or carried by the shaft and
  - 5 remanently magnetised to emanate a component of magnetic field that is dependent on torque applied about said axis,
  - a sensor coil disposed about said element to generate a voltage/current in response to changes in said component,
  - a load connected to said sensor coil to enable a current to circulate in
  - 10 the sensor coil; and
  - a receiver unit remote from said coil and responsive to a field emanated by said sensor coil to generate a torque-dependent signal.
2. A torque transducer as claimed in Claim 1 in which said receiver unit comprises a coil, preferably wound on a magnetic core.
- 15 3. A torque transducer as claimed in Claim 1 in which the receiver unit coil is wound on a ferrite core.
4. A torque transducer as claimed in Claim 1, 2 or 3 in which said load comprises a capacitor connected across said sensor coil to enhance a field component emanated thereby.
- 20 5. A torque transducer as claimed in any preceding claim in which said transducer element comprises a region integral with said shaft and remanently magnetised with an annulus of longitudinal magnetisation (axially-directed magnetisation) which exhibits profile shift, and said sensor coil comprises two spaced coil sections which are aligned with respective

response maxima and are connected such that the voltages induced therein are summed.

6. A torque transducer system comprises a torque transducer which is as claimed in any one of Claims 1 to 5, and wherein said shaft is coupled to or is  
5 a part of a source of a torque pulse, such as a power torque tool.

7. A torque transducer assembly comprising:

a housing having an opening therethrough;

a torque transmission shaft extending in said opening and rotatable about an axis extending through said opening, said shaft having respective  
10 end portions accessible from exteriorly of said housing,

a torque transducer element integral with, or carried by, said shaft to emanate a magnetic field dependent on the torque in the shaft,

a coil coaxial with said element and adjacent thereto; and for sensing the torque-dependent field,

15 a load, preferably a capacitive load, connected across the coil to enable current to circulate therethrough for emanating a field externally of the assembly that is dependent on changes in torque in the shaft.

8. A torque transducer assembly as claimed in Claim 7 in which one end portion of said shaft projects exteriorly of said housing and provides an output  
20 portion of the shaft.

9. A torque transducer assembly as claimed in Claim 7 or 8 in which said housing is configured to enable it to be secured against rotation.

10. A torque transducer assembly as claimed in Claim 9 further comprising a member having a first portion engaged with the housing and second portion



engageable with the body of a power torque tool to secure the housing against rotation with respect to said body.

11. A torque transducer comprising:

a shaft subject to torque about a longitudinal axis;

5 a transducer element integral with or carried by the shaft and remanently magnetised to emanate a component of magnetic field that is dependent on torque applied about said axis,

a sensor coil disposed about said element to generate a voltage/current in response to changes in said component,

10 a power supply unit comprising a rectifier arrangement connected to said sensor coil to derive a unipolar electrical supply from changes of torque sensed by said sensor coil; and

signalling means responsive to voltage/current signals in said sensor coil to transmit the signals in a wire-less manner for remote detection, said

15 signalling means being powered by said electrical supply.

12. A torque transducer as claimed in Claim 11 in which said transducer element comprises a region integral with said shaft and remanently magnetised with an annulus of longitudinal magnetisation (axially-directed magnetisation) which exhibits profile shift, and said sensor coil comprises two  
20 spaced coil sections which are aligned with respective response maxima and are connected such that the voltages induced therein are summed.

13. A torque transducer comprising:

a shaft subject to torque about a longitudinal axis;

a transducer element integral with or carried by the shaft and remanently magnetised to emanate a component of magnetic field that is dependent on torque applied about said axis,

5 a sensor coil disposed about said element to generate a voltage/current in response to changes in said component,

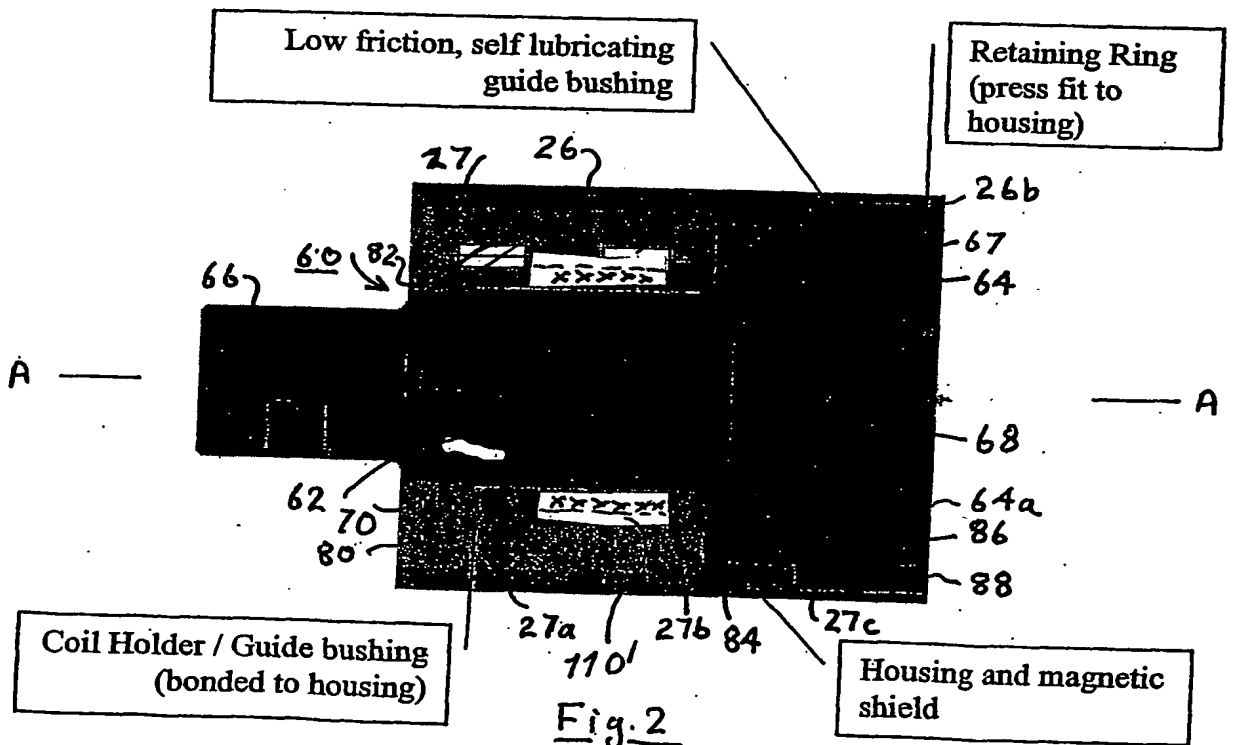
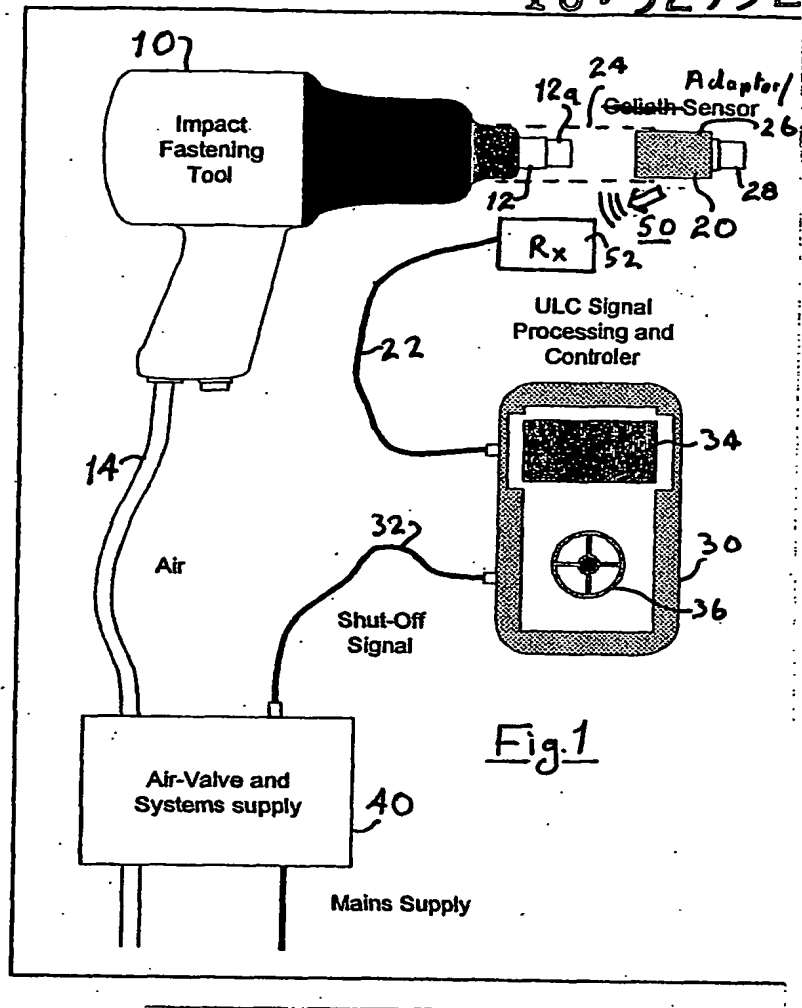
a power supply unit comprising a rectifier arrangement connected to said sensor coil to derive a unipolar electrical supply from changes of torque sensed by said sensor coil;

10 a sensor arrangement responsive to said torque-dependent magnetic field component to provide a torque-dependent signal; and

signalling means responsive to a torque-dependent signal to transmit the signal in a wire-less manner for remote detection, said signalling means and, if appropriate, said sensor arrangement being powered by said electrical supply.

15 14. A torque transducer system comprises a torque transducer which is as claimed in Claim 11, 12 or 13, and wherein said shaft is coupled to or is a part of a source of a torque pulse, such as a power torque tool.

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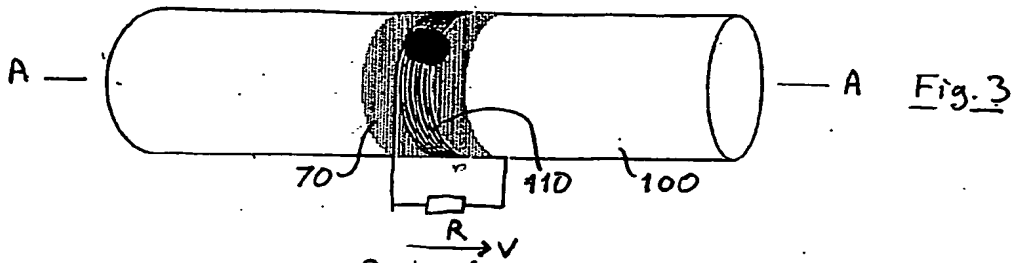


Fig. 3

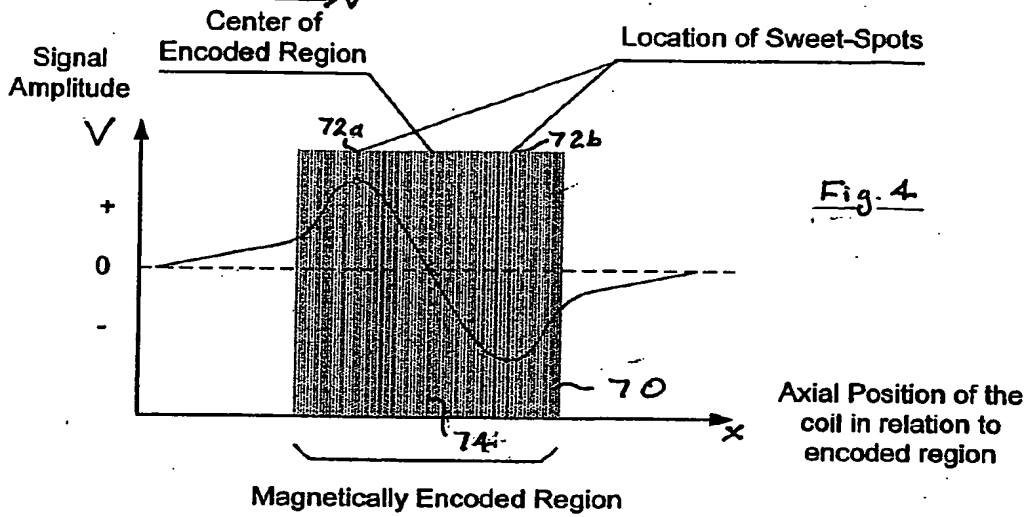


Fig. 4

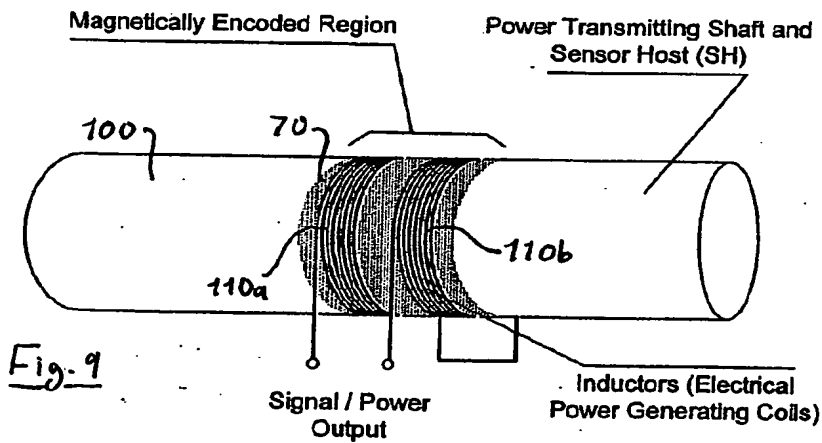


Fig. 9

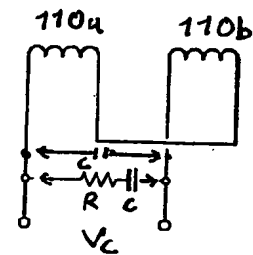


Fig. 9a

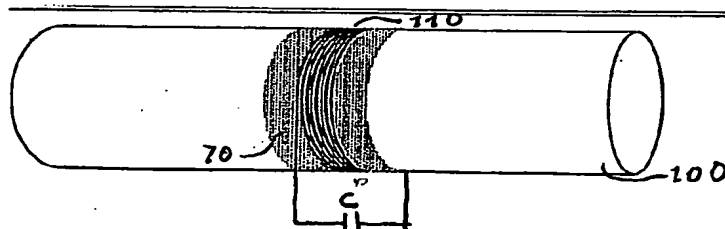


Fig. 6

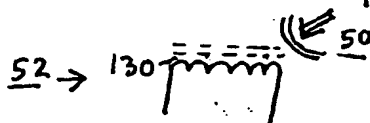
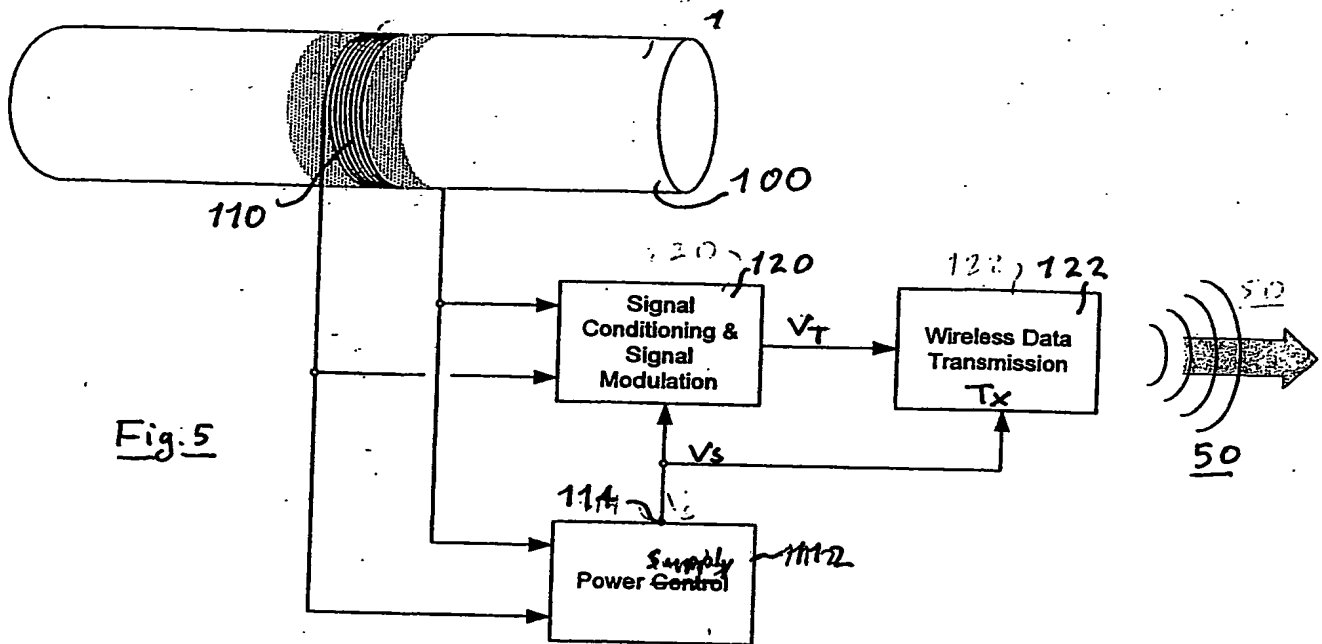


Fig. 6a

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While the inductor remains static.



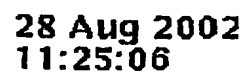


Fig. 7a

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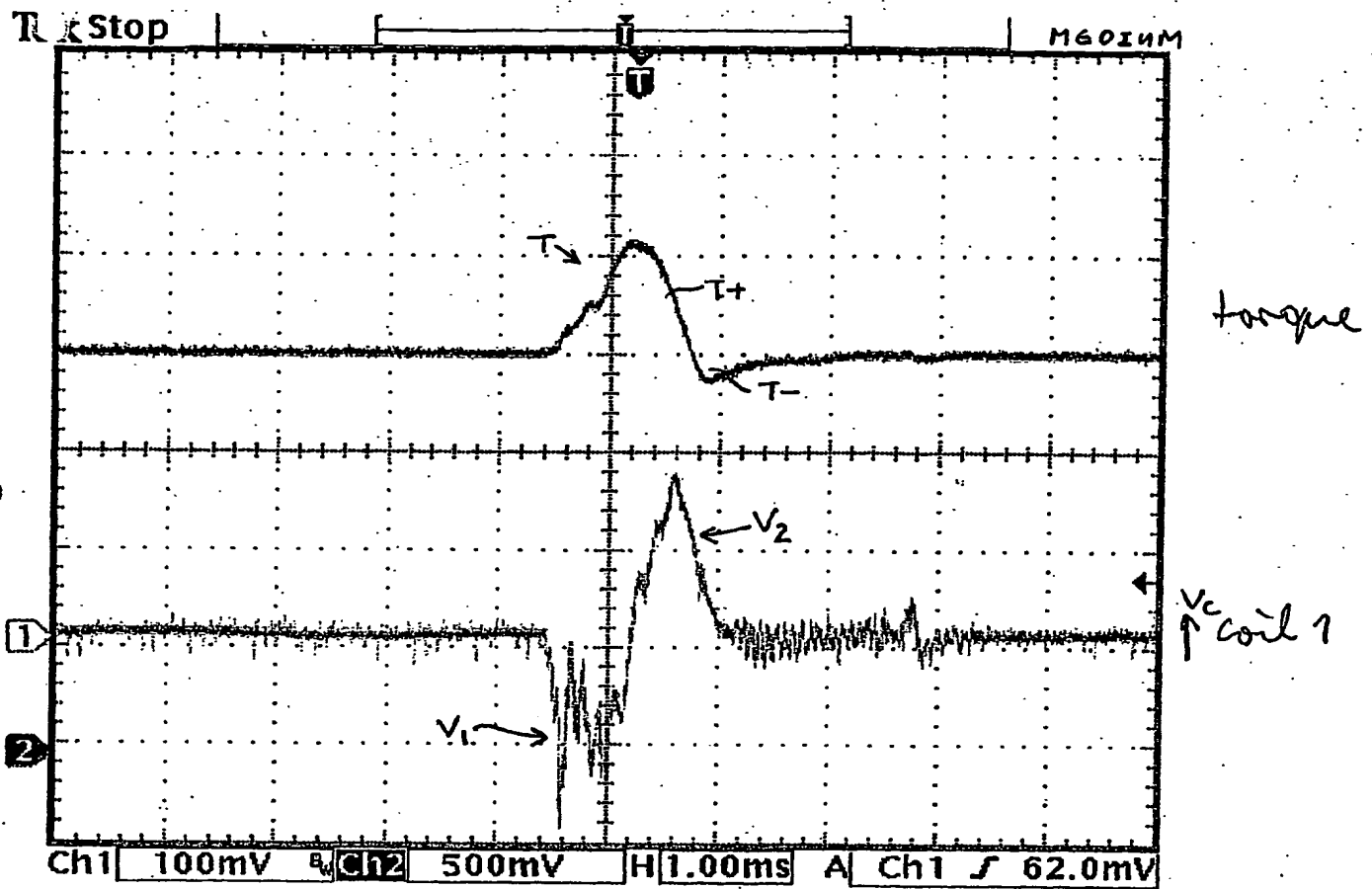
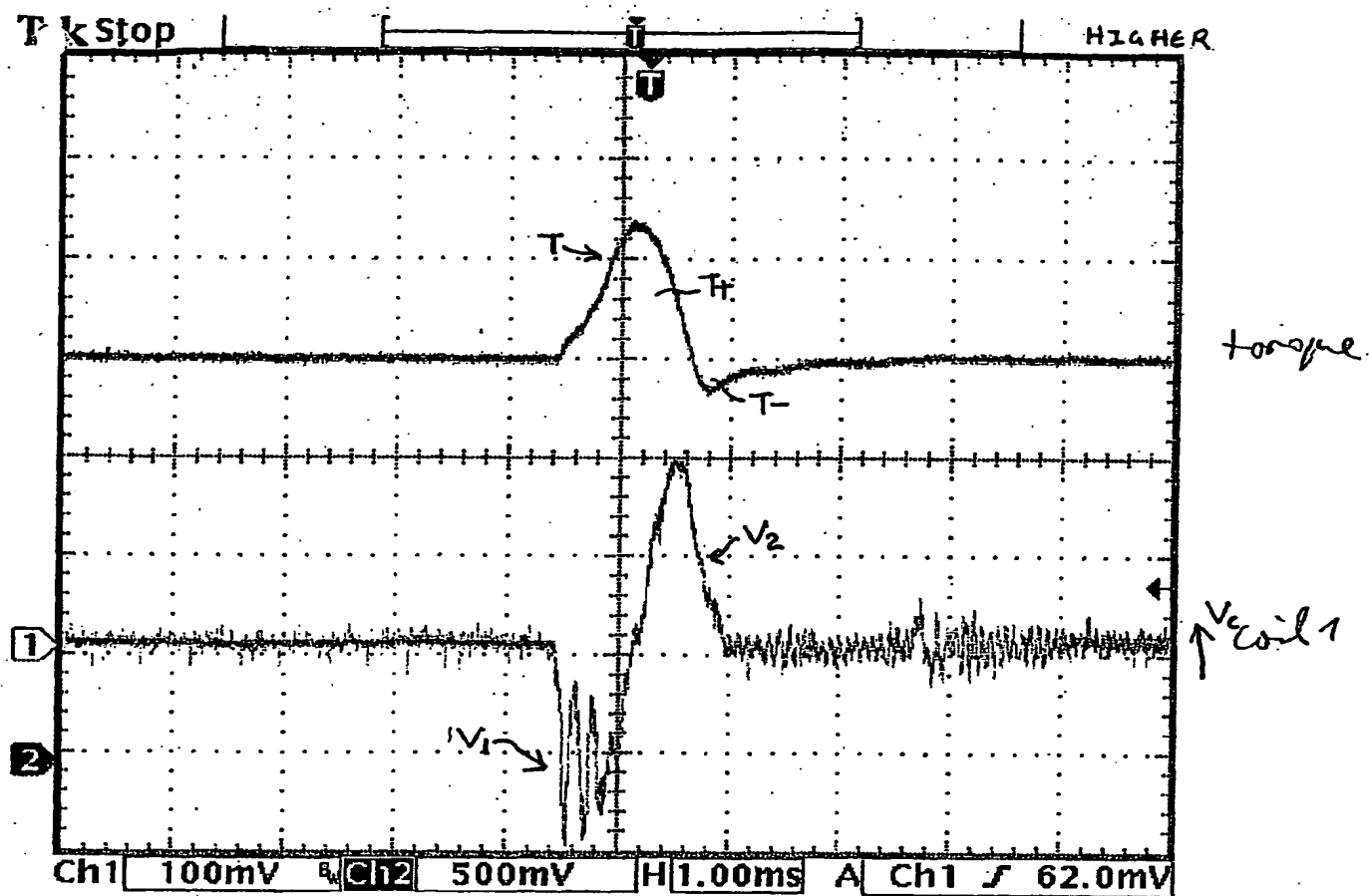


Fig. 7b

52.60 %

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Fig. 7c

52.60 %

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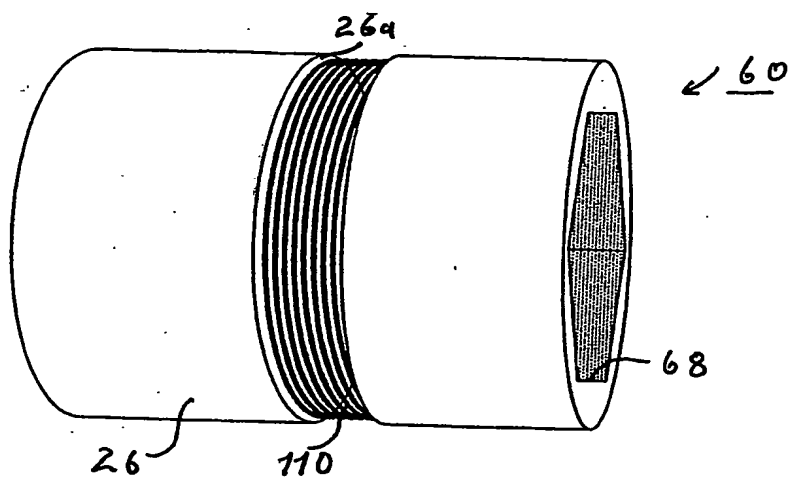


Fig. 8

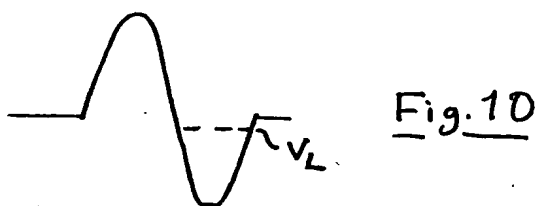


Fig. 10



Fig. 11

# INTERNATIONAL SEARCH REPORT

International Application No  
PCT/EP 03/10634

**A. CLASSIFICATION OF SUBJECT MATTER**  
IPC 7 G01L3/10

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)  
IPC 7 G01L B25B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used).

EPO-Internal, PAJ, WPI Data, INSPEC, COMPENDEX

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 4 882 936 A (GARSHELIS IVAN J) 28 November 1989 (1989-11-28)  column 5, line 29 -column 8, line 32 column 13, line 2 -column 14, line 40 column 22, line 46 -column 26, line 19 figures 1-4,10-12	1-4, 6-11,13, 14
Y	---	5,12
A	EP 0 366 217 A (TOKYO SHIBAURA ELECTRIC CO) 2 May 1990 (1990-05-02) the whole document	1-14
A	US 5 321 985 A (KASHIWAGI YOICHIRO ET AL) 21 June 1994 (1994-06-21) the whole document	1-14
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☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

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- \*&\* document member of the same patent family

Date of the actual completion of the international search

5 February 2004

Date of mailing of the international search report

12/02/2004

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# INTERNATIONAL SEARCH REPORT

International Application No.

PCT/EP 03/10634

## C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
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A	PATENT ABSTRACTS OF JAPAN vol. 007, no. 078 (P-188), 31 March 1983 (1983-03-31) -& JP 58 009034 A (KOUSUKE HARADA; OTHERS: 01), 19 January 1983 (1983-01-19) abstract -----	1, 7, 11, 13

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